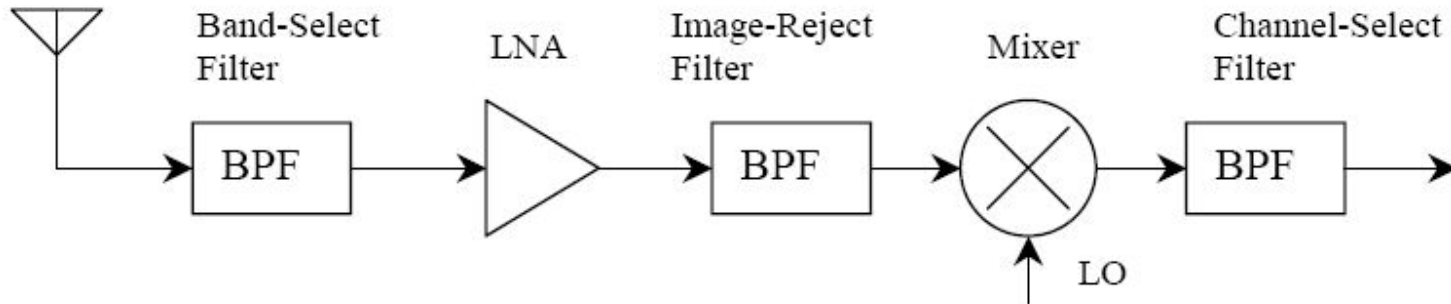


## Up-/Down- conversion in frequency

Why?

- Amplification 120+ dB without parasitic feedback
- Tunable receiver without too many tuned filters
- Easier narrowband filtering

## Superheterodyne receiver



## IF

$$\cos(\omega_1 t)\cos(\omega_2 t) = 1/2 \cos((\omega_1 - \omega_2)t) + 1/2 \cos((\omega_1 + \omega_2)t)$$

$\omega_1 - \omega_2$  - IF or beat frequency

Intermediate frequency is usually lower than RF (easier to amplify/filter/process).

Examples (receivers):

**FM radio:** 88-108MHz  $\longrightarrow$  10.7 MHz

**AM radio:** 150-300kHz, 530-1600kHz, 2.3-26MHz  $\longrightarrow$  465 kHz

**analog TV:** 30 MHz, 45 MHz

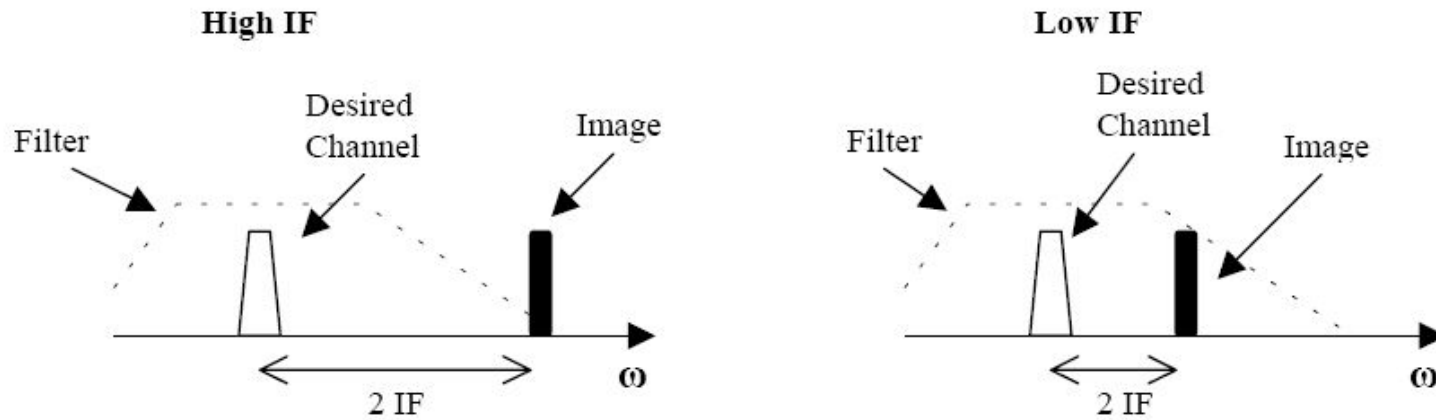
**Satellite equipment:** 10.7-12.75 GHz  $\longrightarrow$  950-1450 MHz first IF (L-band), 70 MHz second IF  
*double conversion receiver!!*

**Terrestrial MW link:** 2.4, 24, 60-70GHz  $\longrightarrow$  250 MHz, 70 MHz

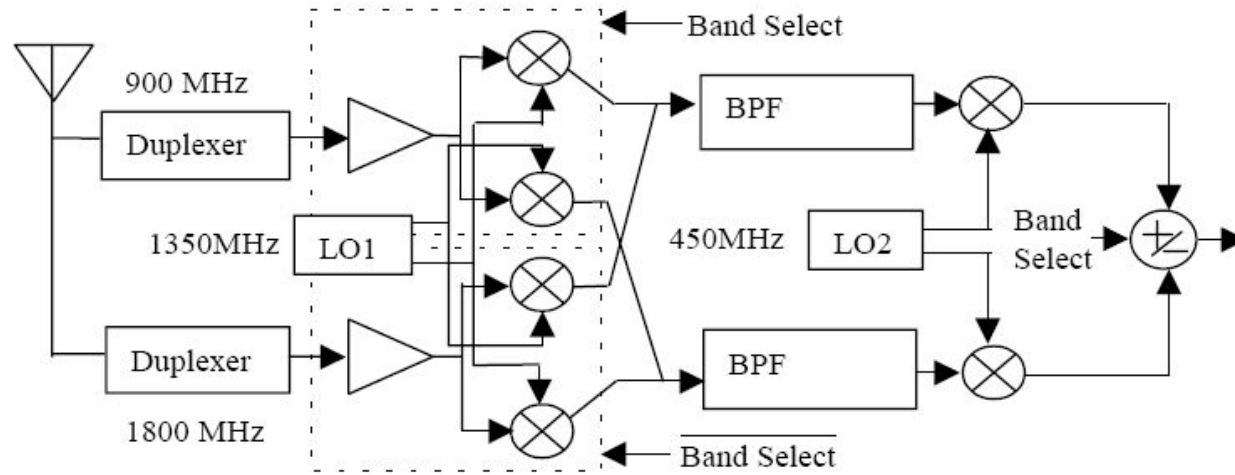
**Radar:** 9.5 GHz  $\longrightarrow$  70 MHz, 30 MHz

## Image band

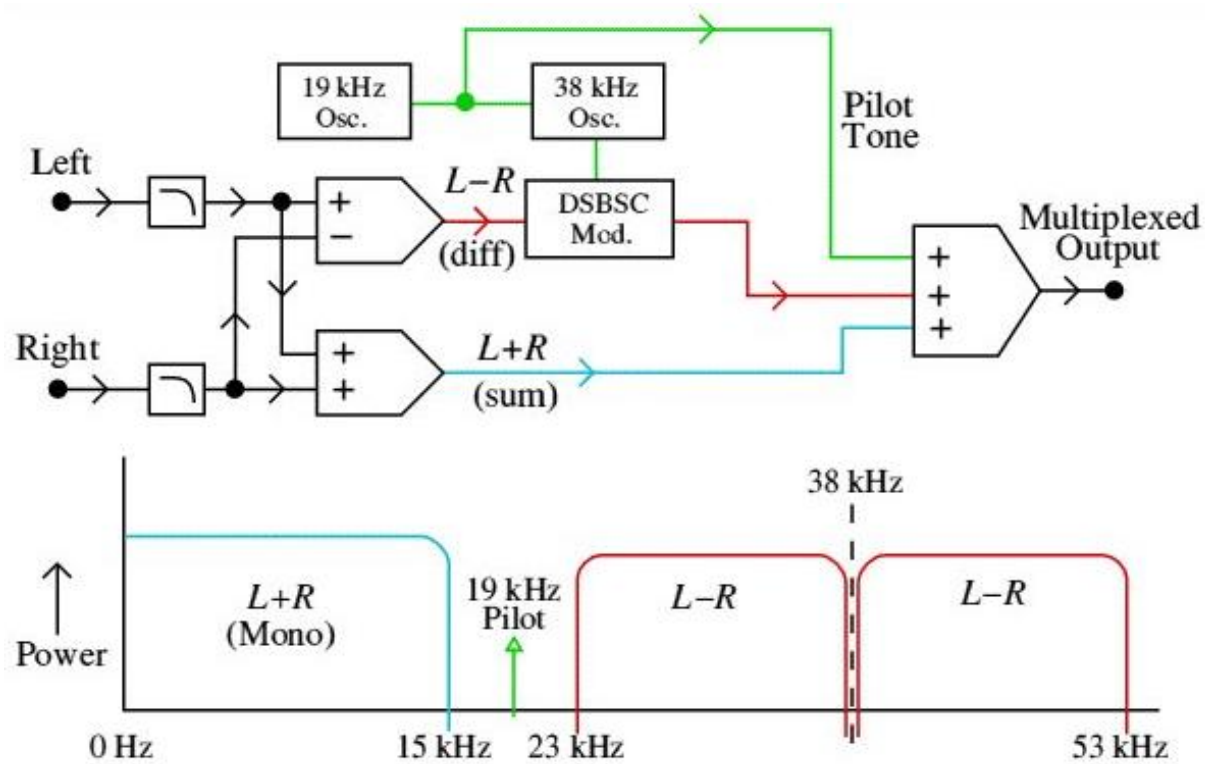
$$f_{RF} = f_{LO} \pm f_{IF} \text{ (which one?)}$$



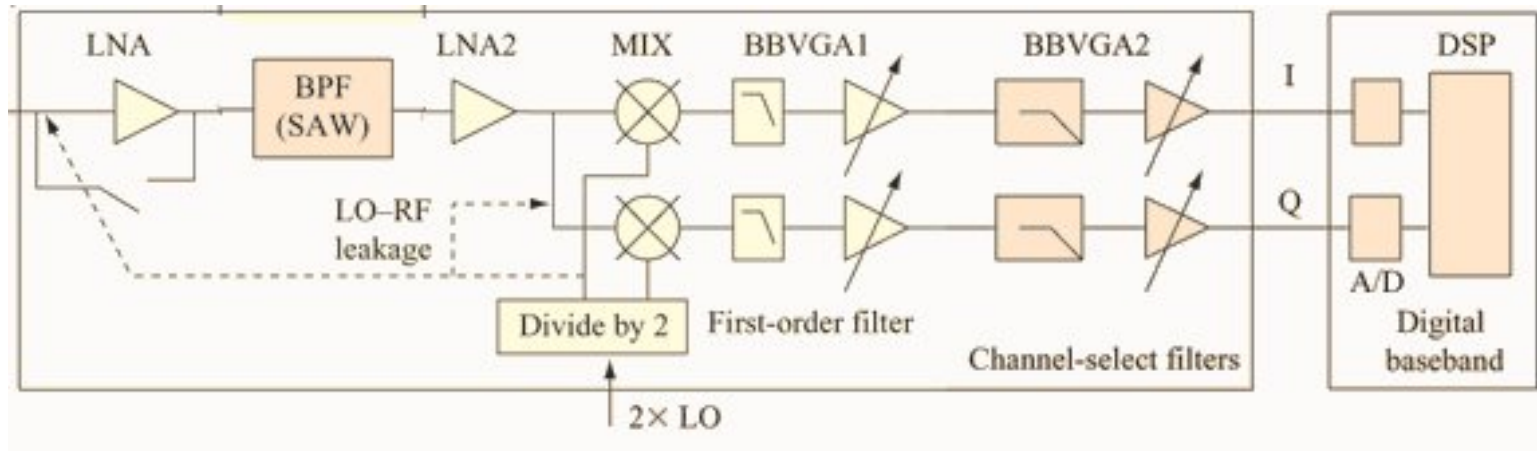
## Dualband receiver example



## Stereo FM example



## Direct conversion receiver (homodyne)



- LO leakage  $\rightarrow$  DC bias  $\rightarrow$  saturation of BB amp
- Linearity (little gain control before mix)
- $2\times LO$  - to produce phase-shifted "sin" & "cos" LO
- Synchronization of LO with carrier (radar  $\rightarrow$  easy, other  $\rightarrow$  PLL, digital cancel, ...)
- no image band!

*Guess what BBVGA stands for....*

## Transmitter - modulation

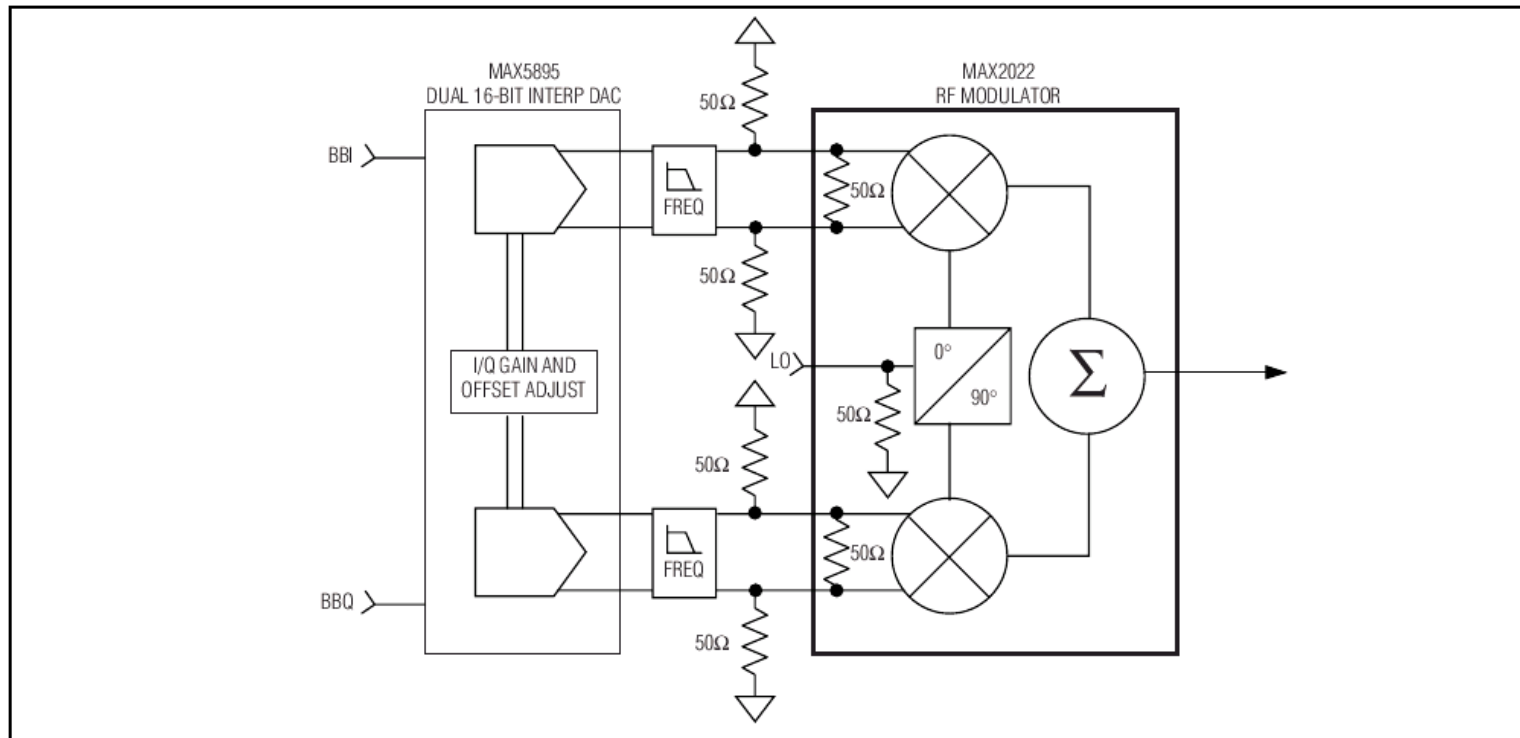
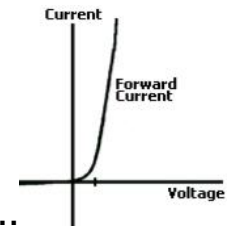
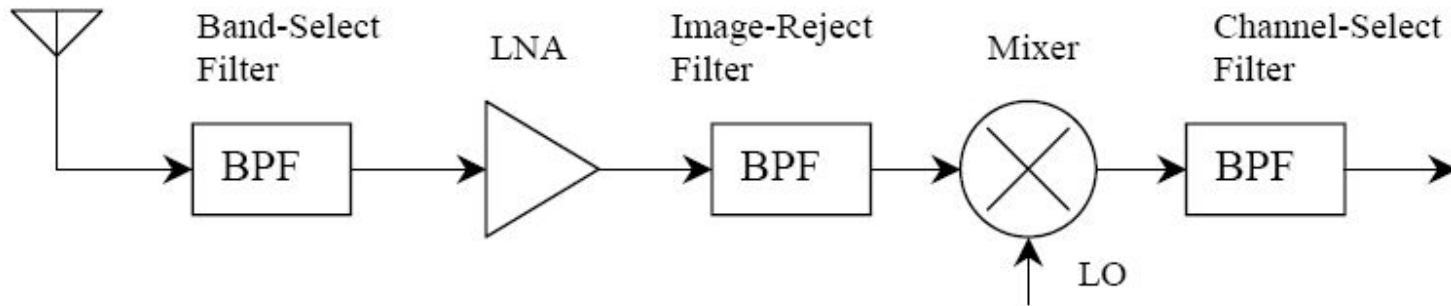


Figure 1. MAX5895 DAC Interfaced with MAX2022

*Why do we need barbecue?*



## Mixer



How to multiply two signals?  $\rightarrow$  use any element with  $x^2$  type nonlinearity...

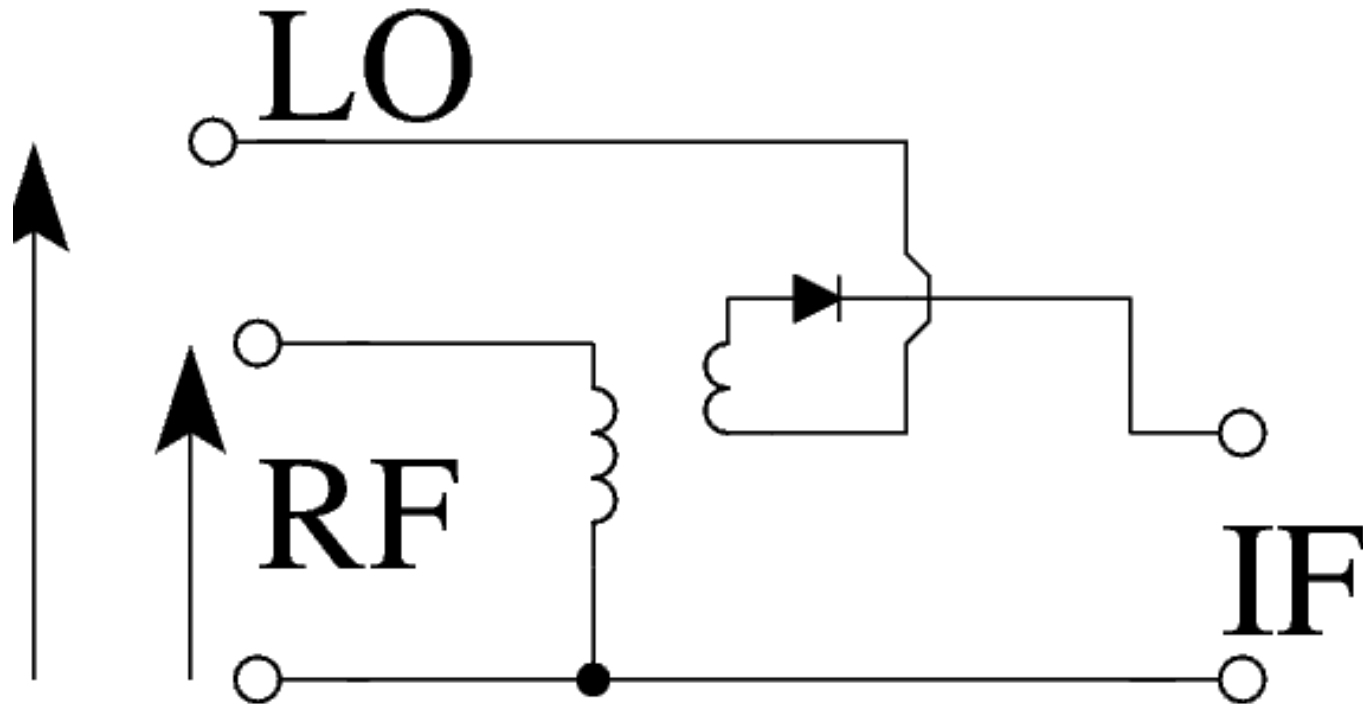
$$(\cos(\omega_1 t) + \cos(\omega_2 t))^2 = \cos(\omega_1 t)^2 + \cos(\omega_2 t)^2 + 2\cos(\omega_1 t)\cos(\omega_2 t)$$

... and filter out  $\cos^2(\omega t) = 1/2 + 1/2\cos(2\omega t)$  components  
(simple but widely used version)

## Diode mixer



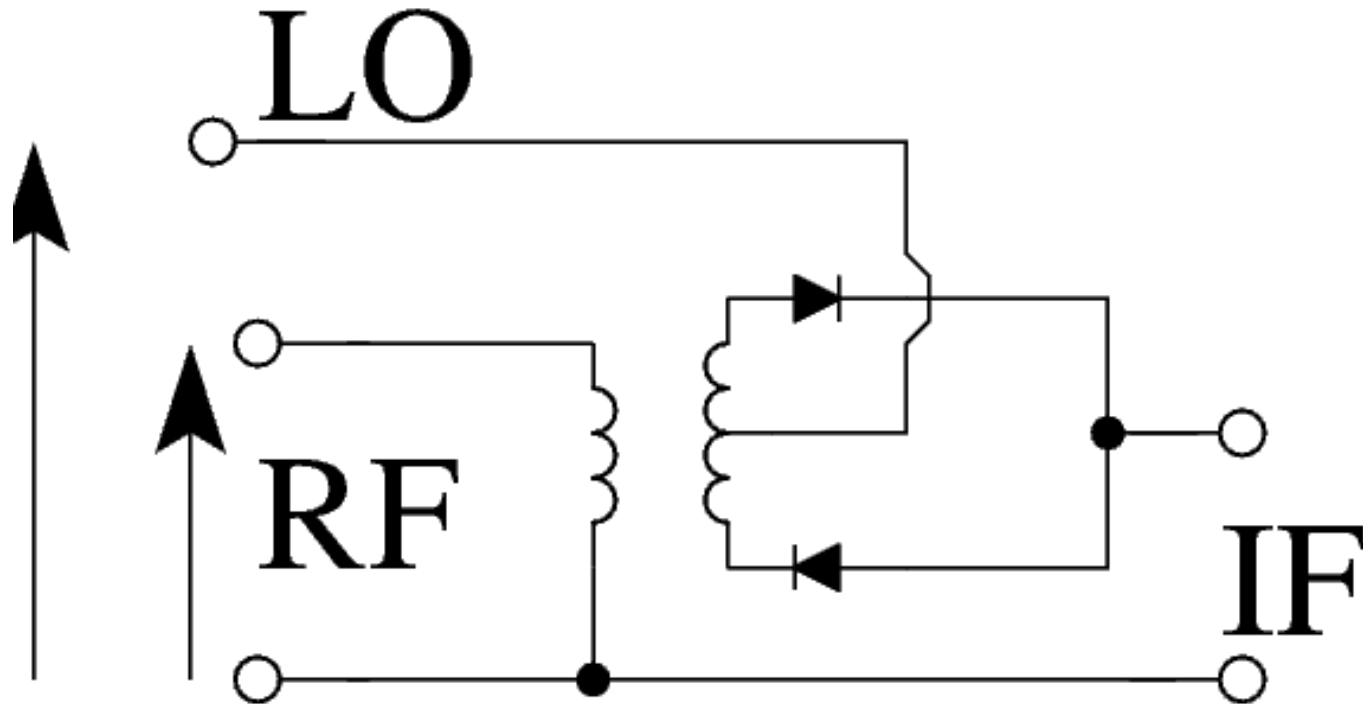
(Simple mixer: works only in the positive half-period)



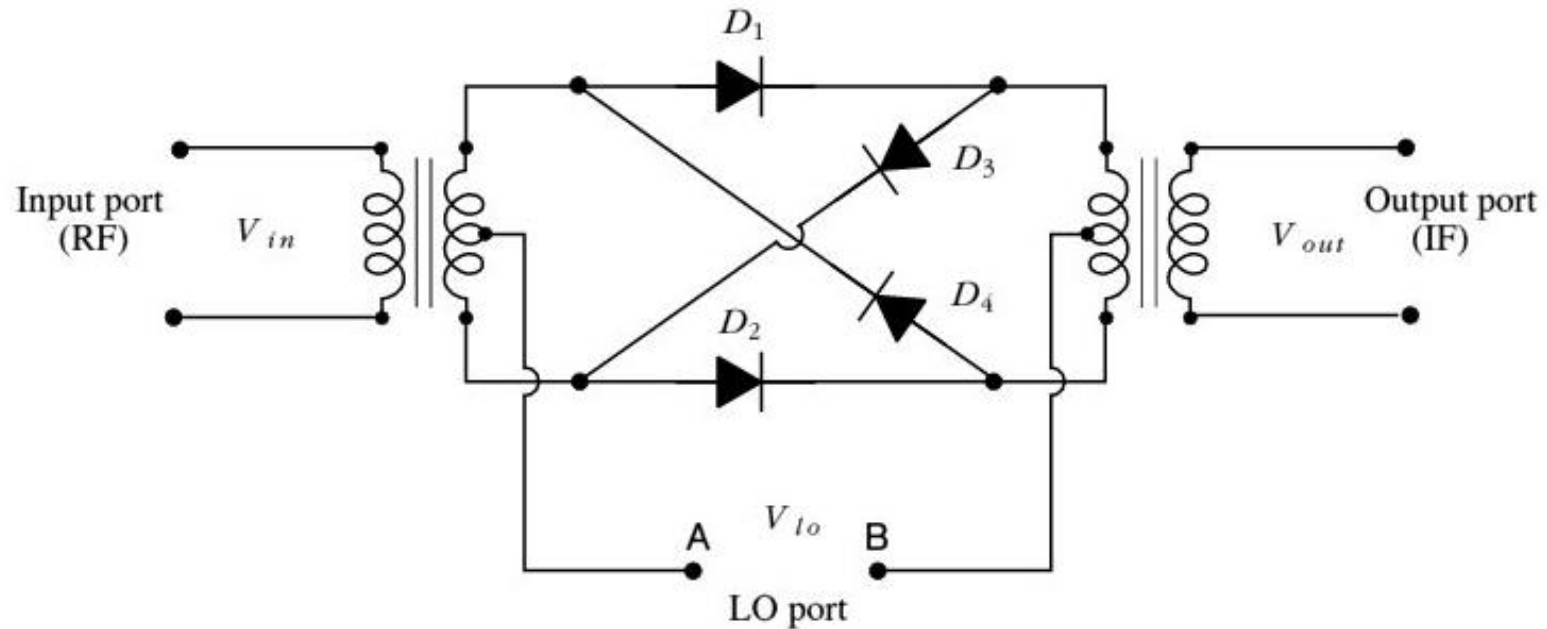
## Single-balanced mixer



(Simple mixer: with symmetrical diodes LO  $\leftrightarrow$  RF leakage minimized)

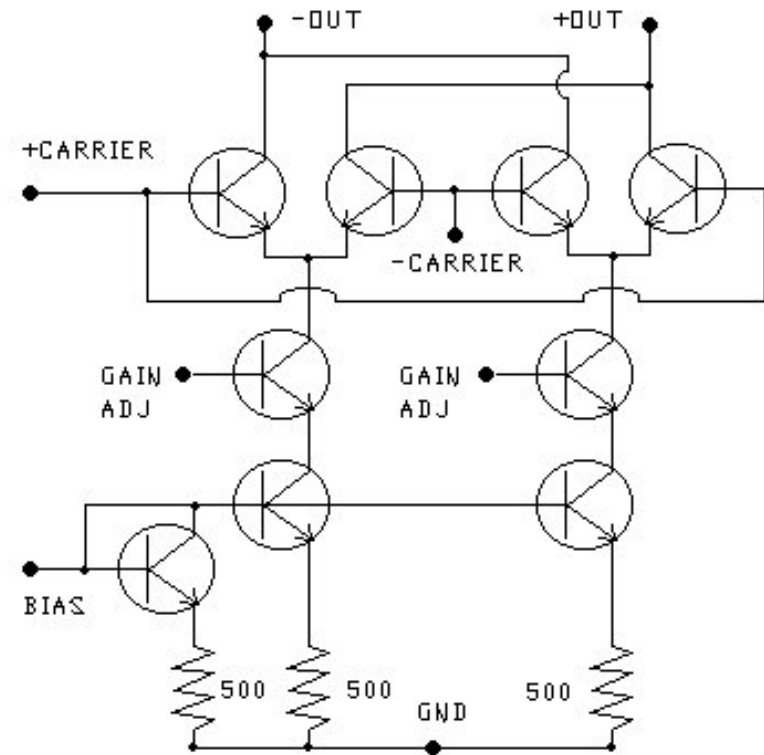
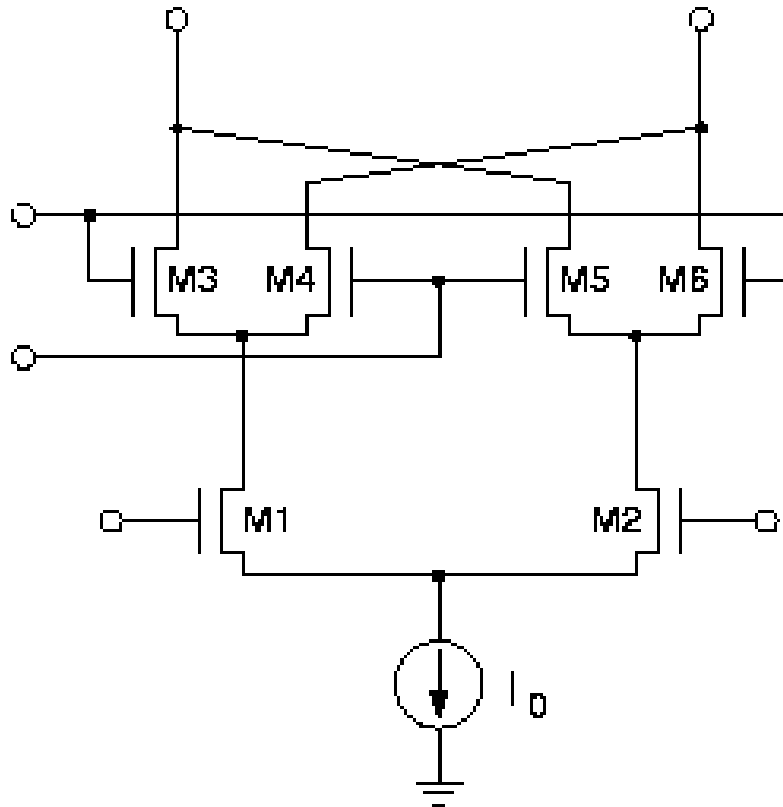


## Balanced diode mixer



(Balanced mixer: works symmetrically vs. the positive and negative half-period)

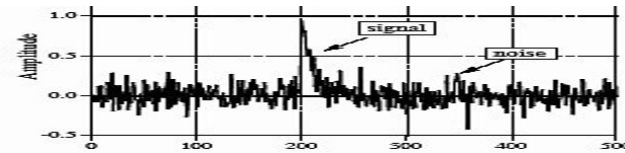
## Balanced mixer circuits



*Try to see the similarity in principle to the 4-diode mixer;  
guess input roles in MOS;  
find bad input markings in bipolar.*

## Matched filter

Task: detect a signal  $s(t)$  in noise.  
*Is There Anybody Out There? (and when?)*



Idea: use LTI filter that maximizes  $peakSNR = (\text{signal instantaneous power}) / (\text{noise power})$  ratio *at some instant* (assume e.g. at  $t = 0$ )

Derivation: assume noise is white with PSD  $N_0$ ; after a filter  $H(j\omega)$  noise power is

$$P_N = N_0 / 4\pi \int_{-\infty}^{+\infty} |H(j\omega)|^2 d\omega$$

After the  $H(j\omega)$  filter the signal spectrum becomes

$$Y(j\omega) = S(j\omega)H(j\omega)$$

thus the signal at  $t = 0$  (by inv. Fourier transf.)

$$y(0) = 1/2\pi \int_{-\infty}^{+\infty} S(j\omega)H(j\omega)e^{j\omega 0} d\omega$$

We want to maximize  $|y(0)|^2/P_n$

Now we put our spectra into the Schwarz inequality:

$$\left| \int S(j\omega)H(j\omega)d\omega \right|^2 \leq \int |S(j\omega)|^2 d\omega \int |H(j\omega)|^2 d\omega$$

so

$$pS/N = \frac{|y(0)|^2}{P_n} = \frac{|\int S(j\omega)H(j\omega)d\omega|^2}{N_0/2 \int |H(j\omega)|^2 d\omega} \leq 2/N_0 \int |S(j\omega)|^2 d\omega$$

If we guess find  $H(j\omega)$  such that the above  $\leq$  becomes  $=$ , nobody will find anything better..

For complex numbers  $|X|^2 = X \cdot X^*$  so

$$\frac{\int S(j\omega)H(j\omega)d\omega \int S^*(j\omega)H^*(j\omega)d\omega}{\int H(j\omega)H^*(j\omega)d\omega} \leq \int S(j\omega)S^*(j\omega)d\omega$$

if we put  $H(j\omega) = S^*(j\omega)$  we got it!  $\rightarrow$  (please recall from circuit theory how we compensate reactive power to maximize power drained from the source)

## Matched filter - conclusions

$$H(j\omega) = S^*(j\omega) \longrightarrow H(t) = S(-t)$$

We may modify it a little bit:

- delay in time by length  $t_s$  of  $s(t)$   $\longrightarrow$  so that  $h_d(t) = h(t - t_s)$  is causal
- scale it by any constant (equality holds)

As now  $|y(0)|^2 = 1/2\pi \int_{-\infty}^{+\infty} |S(j\omega)|^2 d\omega = E =$  signal energy of  $s(t)$  (Parseval),  
pSNR at the output of an ideal matched filter equals

$$pSNR = \frac{2E}{N_0}$$

... but other signal parameters (BW,  $t_s$  ...) may be used for whatever we want. (technical reasons, sidelobes.....)



## Matched filter - improvement factor

How big a peak can we have after a MF?

S/N before & after MF:

$$SNR_{in} = \frac{\overline{x^2}}{BN_0} \quad SNR_{out} = \frac{2E}{N_0}$$

and

$$E = \overline{x^2}t_i$$

so we get improvement by:

$$IF_{MF} = \frac{SNR_{out}}{SNR_{in}} = \frac{2E}{N_0} \frac{BN_0}{\overline{x^2}} = 2Bt_i$$

An alternative explanation:

A signal with a bandwidth B may have a minimum duration of  $1/B$ . So with a best (*matched*) filter we can squeeze a pulse from  $t_i$  to  $1/B \rightarrow Bt_i$  times.....

## Matched filter - variations

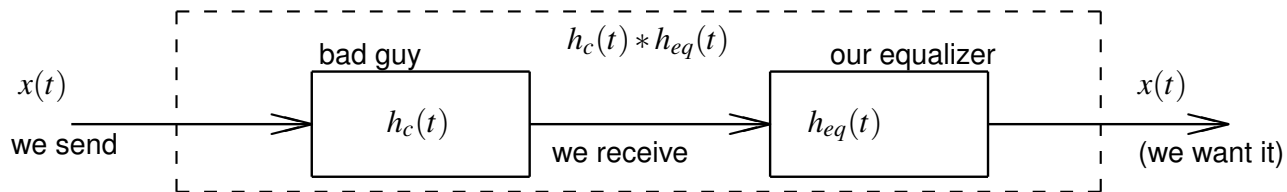
- ...with non-white noise:

$$H(j\omega) = \frac{S^*(j\omega)}{|N(j\omega)|^2} = \frac{1}{N(j\omega)} \cdot \frac{S^*(j\omega)}{N^*(j\omega)}$$

(whitening + matched to a spoiled  $s(t)$ )

- Mismatched filter - a matched filter modified a bit, e.g. to reduce sidelobes:
    - modification by windowing
    - modification by optimization techniques
- **mis**matched filter is not optimal for  $pSNR$ , but by losing a little bit of  $pSNR$  we may make it optimal in some other sense

## Equalizer or Inverse Filter



Somebody (a bad guy the channel) disturbs our signal as a filter  $h_c(t)$ ; we want to compensate for it with  $h_{eq}(t)$  so that  $h_c(t) * h_{eq}(t) = \delta(t)$

In spectral domain:  $H_c(j\omega) \cdot H_{eq}(j\omega) = 1 \longrightarrow H_{eq}(j\omega) = \frac{1}{H_c(j\omega)}$ .

How to know  $h_c(t)$ ? Estimate it using a known signal (e.g. preamble). We may also estimate  $h_{eq}(t)$  using *adaptive filter*.

DANGERS:

- If  $h_c(t)$  is FIR,  $h_{eq}(t)$  is IIR
- When  $H_c(j\omega) = 0$  we have  $1/0$  (trick: use  $H_{eq}(j\omega) = \frac{1}{H_c(j\omega)+k}$  with small  $k > 0$ ).
- Zeros of  $H_c(s)$  become POLES of  $H_{eq}(s)$  (tricks needed to ensure stability).

## Filters - summary

- Matched filter - maximize pSNR,  $h(t) = s(-t)$ 
  - mismatched filter - matched filter with some modifications
- Whitening filter - change non-white noise to white,  $H(j\omega) = 1/N(j\omega)$
- Equalization filter or *inverse filter* - compensate the  $F(j\omega)$  of a channel:  $H(j\omega) = 1/F(j\omega)$